

Client:	VHR Roof Tile Mfg.	Report Date: 8/3/18
	1665 Bohm Drive	ATLSF Report #: RT0803.01-18
	Little Chute, Wisconsin 54140	
	Att. Bruce Rouleau	
Re:	Calculations for Restoring Moment Due to Gravity and Aerodynamic Multiplier	
References:	Florida Building Code, 6 <sup>th</sup> Edition (2017), section 1518.8.5; TAS 101-95, sections 10.1	
	& 10.2; TAS 102/102A, sections 9.1 &	2 9.2.

Test Authorized by:	Bruce Rouleau	
Sampled by:	Client	
Date of Receipt:	8/1/18	
ATLSF Item #:	112461	
Referenced Test Method:	Florida Building Code, TAS 101-95	
Manufacturer:	VHR Roof Tile Mfg.	
Model:	Flat Profile, Concrete Roof Tile	
Quantity Received:	6 tiles	
Nominal Dimensions (in.):	Specified by Supplier:15.375 x 10.625 x 0.938	
(l x w x h):	Measured: 15.0 x 10.5 x 1.1	
Nominal Weight (lbf):	8.5	
specified by supplier:		
Imprint:	VHR – on the underside, at the nose end of the tile	
Classification:	FBC TAS 112-95: Type 3a- Flat Profile, Interlocking, Class III	
	ASTM C1492-03: Type II- Medium Profile, Interlocking,	
	Normal Weight	

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Calculations:

- Weight (W): (Weight obtained from ATLSF Report #: RT0618.02-18) W = m x <u>1 lbf s<sup>2</sup>/ft x</u> 32.2 ft/s<sup>2</sup> 32.174 lbm W = 8.5 x 1.0008 W = 8.507 lbf
- 2. Restoring Moment Due to Gravity (Mg): (α: determined from mock-up layout in laboratory)

Direct Deck Application  $M_g = W \ x \ cos \ (\theta - \alpha) \ x \ L_g$   $M_g = 8.507 \ cos \ (9.462^\circ - 5.410) \ x \ 0.641$  $M_g = 5.439 \ ft-lbf$ 

Pitch	Equation	Restoring Moment Due to Gravity (Mg)
2:12	$M_g = 8.507 \text{ x cos} (9.462 - 5.410) \text{ x } 0.641$	$M_{g} = 5.44$
3:12	$M_g = 8.507 \text{ x cos} (14.036 - 5.410) \text{ x } 0.641$	$M_{g} = 5.39$
4:12	$M_g = 8.507 \text{ x cos} (18.435 - 5.410 \text{ x } 0.641$	$M_{g} = 5.31$
5:12	$M_g = 8.507 \text{ x cos} (22.620 - 5.410) \text{ x } 0.641$	$M_{g} = 5.21$
6:12	$M_g = 8.507 \text{ x cos} (26.565 - 5.410) \text{ x } 0.641$	$M_{g} = 5.08$
7:12	$M_g = 8.507 \text{ x cos} (30.256 - 5.410) \text{ x } 0.641$	$M_g = 4.95$

## **Batten Application**

$$\begin{split} M_g &= W \; x \cos \left( \theta - \alpha \right) x \; L_g \\ M_g &= 8.507 \; \cos \left( 9.462^\circ - 5.410 \right) x \; 0.500 \\ M_g &= 4.243 \; \text{ft-lbf} \end{split}$$

Pitch	Equation	Restoring Moment Due to Gravity (Mg)
2:12	$M_g = 8.507 \text{ x cos} (9.462 - 5.410) \text{ x } 0.500$	$M_{g} = 4.24$
3:12	$M_g = 8.507 \text{ x cos} (14.036 - 5.410) \text{ x } 0.500$	$M_{g} = 4.21$
4:12	$M_g = 8.507 \text{ x cos} (18.435 - 5.410 \text{ x } 0.500$	$M_{g} = 4.14$
5:12	$M_g = 8.507 \text{ x cos} (22.620 - 5.410) \text{ x } 0.500$	$M_{g} = 4.06$
6:12	$M_g = 8.507 \text{ x cos} (26.565 - 5.410) \text{ x } 0.500$	$M_{g} = 3.97$
7:12	$M_g = 8.507 \text{ x cos} (30.256 - 5.410) \text{ x } 0.500$	$M_{g} = 3.86$

- 3. Aerodynamic Multiplier ( $\lambda$ ): For Direct Deck Application: b = 9.75''/12: 1 = 12''/12  $\lambda = 0.156 \text{ x b x } 1^2$ :  $\lambda = 0.156 \text{ x } 0.813 \text{ x } 1.000^2$  $\lambda = .13$
- 4. Aerodynamic Multiplier ( $\lambda$ ): For Batten Application: b = 9.75"/12: l = 12"/12  $\lambda$  = 0.144 x b x l<sup>2</sup>:  $\lambda$  = 0.144 x 0.813 x 1.000<sup>2</sup>
  - $\lambda = .12$

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The above calculations were conducted in compliance with Florida Building Code sections referenced above with the values based on our laboratory measurements. Static uplift testing was not performed. It is our understanding that the client is a member of the Tile Roof Institute and that Uplift Resistance Values will obtained from their file data.

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End of report.

Prepared by:

Tony Porcello, RRO President American Test Lab of South Florida

